

Description

5 Vertical laser diode with beam profile shaping

The invention relates to a laser diode with a vertical resonator according to the precharacterizing clause of claim 1 and to an optical system with such a laser diode according to
10 claim 14.

Vertical laser diodes are known, for example, in the material systems of InAlGaAsN or InAlGaP on a GaAs substrate, InAlGaAsP on an InP substrate or InAlGaAsN on a sapphire or SiC
15 substrate and are described in their essential features in K. J. Ebeling, Integrated Optoelectronics, Springer Verlag 1993.

It is characteristic of these vertical laser diodes that the vertical laser diodes contain active multiquantum well layers
20 for light generation and Bragg reflectors integrated in a monolithic or hybrid manner, which form the optical Fabry-Perot resonator. For current constriction in the vertical laser diode, selective lateral oxidation, proton implantation or mesa etching are used, which along with thermal effects
25 also determine the optical wave guidance in the structures.

In the case of the known vertical laser diodes, it is disadvantageous that the structure-induced transverse mode selection is not particularly efficient, so that pure emission
30 on the transverse fundamental mode can be observed only in structures with small diameters and at comparatively low output power levels.

The object of the present invention is to specify a vertical laser diode structure which permits stable beam profile shaping.

- 5 This object is achieved according to the invention by a laser diode with the features of claim 1.

An essential part of the invention is the introduction of a means for beam profiling, the means having at least one
10 absorber means with a decoloring (saturable) absorber.

The at least one decoloring absorber means favors emission of the dominant transverse mode with highest optical intensity (for example transverse fundamental Gaussian mode with its
15 intensity maximum on the axis), since the decolouring of the absorber is at its greatest at the locations of greatest intensity.

Decoloring absorbers or decoloring quantum films are known per
20 se as optical absorbers with nonlinear absorption behavior. The transmission of the decoloring absorbers depends on the irradiated radiation intensity. With increasing power densities, the absorption decreases; at very high power densities, the absorber is substantially transparent. The use
25 of absorber means for semiconductor lasers is known in principle (for example from US-A-5,574,738), these absorber means only being used to absorb certain wavelengths of the radiation, to achieve self-modulation of the laser diode in the GHz range.

30 The invention is concerned with the fact that light in the vertical resonator has in principle an inhomogeneous intensity distribution over the beam cross section, the decoloring absorber means ensuring that the light is attenuated only

little at the locations of high intensity in the absorber means.

Consequently, absorption losses of the dominant transverse
5 mode (for example transverse fundamental Gaussian mode) in
laser diodes with a vertical resonator can be kept
particularly small, so that the emission on this transverse
mode (for example the fundamental mode) is favored.
Consequently, beam profiling is achieved in an efficient way.

10 With suitable setting of the fundamental absorption for low
light power levels and the current-dependent optical
amplifiers in the laser, self-pulsations and also optical and
electrical bistability can occur.

15 This form of operation is preferred in optical scanning
systems, for example in a CD player. In addition, the local
charge carrier generation by absorption in the decoloring
absorber means has the effect of promoting the current
20 injection near the axis of the active zone, which in turn is
advantageous for the fundamental mode emission.

Use of the laser diode according to the invention also allows
the dynamic performance of the switching-on and switching-off
25 operation of optical data transmission devices to be improved.
In these operations, the build-up of oscillations of other, in
particular higher, transverse modes occurs. Use of a
decoloring absorber means in the laser diode stabilizes the
emission on the dominant transverse mode (for example
30 transverse fundamental mode) and consequently prevents the
undesired occurrence of pattern effects in the transmission of
digital signal sequences. As a result, higher data
transmission rates and a more stable mode behavior can be
achieved over a wide temperature range. Furthermore,

fundamental mode operation is consequently possible with larger component dimensions, so that the required production tolerances are reduced.

5 In an advantageous configuration of the present invention, a pn junction of III-V or II-VI compound semiconductor material is used, since these materials are well suited for vertical laser diodes.

10 To make production simple, at least one absorber means is integrated monolithically into a series of layers.

For particularly efficient beam profiling, it is advantageous if at least one absorber means is arranged in the Fabry-Perot resonator of the series of layers of the vertical laser diode. 15 The absorber and amplifier quantum films then advantageously lie in the beam waist of the Gaussian beam and ensure an optimum transverse mode selection.

20 Furthermore, it is advantageous if at least one absorber means is arranged outside the depletion zone of the pn junction.

In a further advantageous configuration of the laser diode according to the invention, at least one decoloring absorber means is formed as a layer in the vertical resonator, the 25 thickness of the layer being small, approaching a quarter of the material wavelength. It is also advantageous if at least one absorber means is formed as a layer with the thickness of the layer being greater than a quarter of the material wavelength. Selection of the layer thickness of one or more 30 layers allows the absorption behavior to be varied.

It is advantageous if at least one absorber means has a means of current constriction, in particular by combination of the

medium of the absorber means with an oxide aperture or a proton implantation. The transverse mode selection can be assisted in this way.

- 5 It is likewise advantageous if the laser diode according to the invention has two electrical supply leads, one for the p contact and one for the n contact.

- 10 In an advantageous way, an embodiment of the laser diode has a current constricting means in the vertical resonator.

- 15 A further improvement of the mode selection can be achieved if, in an advantageous way, at least one reflective layer in the vertical resonator has a relief structure, in particular a Fresnel lens.

- At least one spacer layer is arranged with advantage in the vertical resonator, in particular between the absorber layer and the active zone.

- 20 Furthermore, it is advantageous for influencing the emission wavelengths if at least one layer of the vertical resonator consists of GaAsN or InGaSbP.

- 25 The laser diode according to the invention is advantageously used in optical systems, in particular in CD players and data transmission systems.

- 30 The invention is explained in more detail below on the basis of several exemplary embodiments, with reference to the figures of the drawings, in which:

figure 1 shows a schematic representation of an embodiment of the vertical laser diode according to the invention;

figure 2 shows a schematic representation of the vertical laser diode according to the invention as a detail from figure 1.

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The structure outlined in figure 1 of a vertical laser diode with an integrated decoloring absorber layer 50 with an absorber means 5 has, as the lowermost layer, an n-doped GaAs substrate 1, which is provided with a GeNiAu contact 10.

10

An approximately 4 μm thick, first $\text{Al}_{0.7}\text{GaAs}_{0.3}$ -GaAs Bragg reflector 2, with a doping of $n=1 \cdot 10^{16} \text{ cm}^3$, is grown onto the GaS substrate.

15

Arranged above the Bragg reflector 2 is an n-doped ($n=5 \cdot 10^{17} \text{ cm}^3$) $\text{Al}_{0.3}\text{Ga}_{0.7}\text{As}$ carrier capture layer 3 and arranged over that is an undoped active zone 4. The active zone 4 has three 8 nm thick quantum films 4a with approximately 50 nm thick GaAs boundary layers 4c and 10 nm thick GaAs barriers 4b (see in detail of figure 2).

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Located above the active zone 4 is an $\text{Al}_{0.3}\text{Ga}_{0.7}\text{As}$ carrier capture layer 51, not represented here in detail, which has a doping of $p=5 \cdot 10^{17} \text{ cm}^3$ (see figure 2). This carrier capture layer 51 is assigned here to the identically doped absorber layer 50 (figure 2).

25

Arranged in the absorber layer 50 as the decoloring absorber means 5 is an 8 nm thick $\text{In}_{0.2}\text{Ga}_{0.8}\text{As}$ quantum film. This is surrounded on both sides by in each case 10 nm thick GaAs barriers, these layers all having a doping of $p = 5 \cdot 10^{17} \text{ cm}^3$ (see figure 2).

30

Serving as the decoloring absorber means 5 as such is the $\text{In}_{0.2}\text{Ga}_{0.8}\text{As}$ quantum film. The transparency of the absorber means 5 increases with increasing irradiation intensity, so that at high intensities the absorber means is substantially transparent. In the case of such quantum films, the intensity critical for the decoloring lies around 1 kW/cm^2 .

The absorber layer 50 may be arranged in the p-doped or n-doped region of the cladding layer. If a plurality of absorber layers 50 are used, they can be arranged in both regions of the cladding layer.

The strength of the desired absorption can be specifically set by the material composition and the thickness and position of the absorber layer(s) 50 in relation to the nodes and antinodes of the standing wave field 100 (see figure 2).

Arranged on the absorber layer 50 is an approximately $4 \mu\text{m}$ thick second $\text{Al}_{0.7}\text{Ga}_{0.3}\text{As}$ -GaAs Bragg reflector 6, doped with $p=1 \times 10^{18} \text{ cm}^{-3}$.

This is finished off by a 10 nm thick p^{++} doped GaAs contact layer 7, to ensure a low-impedance connection to the p contacts by means of a TiPtAu contact 20.

Figure 2 shows the structure of the stack of layers between the two Bragg reflectors 2, 6 according to figure 1 as a detail.

The compositions of the layers is reproduced by the scale on the right-hand edge of figure 2. The variables x and y specify here the composition of the respective compound semiconductor $\text{Al}_x\text{Ga}_{1-x}\text{As}$ or $\text{In}_y\text{Ga}_{1-y}\text{As}$.

At the upper edge of figure 2, the assignments of the layers to figure 1 are specified, the layers being indicated by vertical broken lines. The thickness of the layers is specified by dimensions. Furthermore, the optical standing wave field 100 that forms is represented. The thicknesses of the layers are adapted to the standing wave field.

At the lower edge of figure 2, the dopings of the layers are specified. The region A is n-doped, the region B is undoped, the region C is p-doped.

Arranged on the left-hand side of the series of layers is the first Bragg reflector 2, arranged on right-hand side is the second Bragg reflector 6.

In the middle of the series of layers lies the active zone 4, which has three $\text{In}_{0.8}\text{Ga}_{0.2}\text{As}$ quantum films 4a, which are in each case 4 nm wide. The active zone 4 also has 10 nm thick GaAs barriers 4b and on both sides approximately 50 nm thick GaAs boundary layers 4c.

Arranged between the absorber means 5 and the active zone 4 is the $\text{Al}_{0.3}\text{Ga}_{0.7}\text{As}$ carrier capture layer 51, which has a doping of $p = 5 \cdot 10^{17} \text{ cm}^{-3}$.

The absorber means 5 has an 8 nm thick $\text{In}_{0.2}\text{Ga}_{0.8}\text{As}$ quantum film 5a with 10 nm thick GaAs barriers on both sides, which altogether have a doping of $p = 5 \cdot 10^{17} \text{ cm}^{-3}$. In an alternative configuration, the decoloring absorber means 5 may be undoped.

The relative position of the decoloring absorber means 5 in the standing wave field 100 determines the critical average intensity which is necessary for reaching the transparent state.

The $\text{Al}_{0.3}\text{Ga}_{0.7}\text{As}$ cladding layer 52 lying over the upper GaAs barrier is p-doped to the same degree as the carrier capture layer 51.

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Arranged adjoining to the right in figure 2 is a layer 54 for increasing the reflectivity of the Bragg reflector.

There follows an approximately 30 nm thick p-doped AlAs layer 10 53, which after selective oxidation serves for the lateral current constriction in the component.

The active quantum films for light emission are located in an antinode of the optical standing wave field 100 in a depletion 15 zone of the pn junction.

The structure described can be produced in a known way, for example using proton implantation or selective oxidation, as a vertical laser diode. The series of layers described can be 20 realized, for example, by molecular beam epitaxy. Carbon may be used, for example, for the p doping, Si for the n doping. Production is also possible with metal organic vapor phase epitaxy.

25 The saturable absorber layer according to the invention is particularly well suited for monolithic integration and is thereby advantageous for high optical output power in the transverse fundamental mode. The structure also allows the self-pulsating operation of vertical laser diodes. The 30 carrier lifetime in the saturable absorber, which can be set by the doping or crystalline morphology or composition of the latter, allows the saturation intensity of the absorber to be set and also the characteristic period of the self-oscillation to be regulated.

Alternative forms of construction than the configuration outlined, with a plurality of thin decoloring absorber layers or solid saturable structures, are of course possible.

5 Similarly, the structure is not restricted to the InAlGaAs semiconductor system, but can also be realized for example in the material systems of InGaAsP (for example on an InP substrate) or InAlGaAsN (for example on a sapphire, SiC or GaAs substrate). The vertical laser structure can also be
10 realized in II-VI semiconductor systems, such as ZnMgBeS₂Se for example.

Depending on the emission wavelength, GaAsN, InGaAsP, InAlGaAs or InGaAsSbN may also serve as the absorber means 5.

15 To improve the mode selection, relief structures (for example Fresnel lenses) can also be used in the mirror layers. Modulation dopings may also contribute to improving the mode selection.

20 The introduction of spacer layers, in particular between the active zone 4 and the absorber means 5, improves the mode selection.

25 In the embodiment described here, only one absorber means is used in the vertical resonator. It is also possible in principle, in alternative embodiments, to use the principle of transverse mode selection for integrating a plurality of decoloring or saturable absorber means. This is appropriate
30 in the case in which, for example, a plurality of active layers are provided in a stack of layers, as occurs in the case of a multistage vertically emitting laser diode (cascaded laser diode). In cascaded laser diodes, the active regions are electrically coupled with one another by tunnel diodes

operated in the reverse direction, thereby achieving a higher optical gain in the vertical resonator.

5 The increased optical gain in the vertical resonator leads to an improved mode selection in the integrated absorber media.

In any event (i.e. in the case of one or more absorber means 5), the optical decoloring of the absorber can be additionally assisted by local current constriction.

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P-doped, n-doped or undoped layers may be used as layers of the absorber means 5. A combination of doped (for example pn, pin) layers may also be used. The absorber medium may be integrated at any desired points in the laser structure (for
15 example into one of the tunnel diodes).

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The invention is not restricted in its implementation to the preferred exemplary embodiments specified above. Rather, a number of variants which also make use of the laser diode according to the invention in fundamentally different configurations are conceivable.

List of designations

	1	n-doped GaAs substrate
	2	first Bragg reflector
5	3	carrier capture layer
	4	active zone
	4a	In _{0.8} Ga _{0.2} As quantum films
	4b	GaAs barrier
	4c	GaAs boundary layer
10	5	decoloring absorber means
	6	second Bragg reflector
	7	GaAs contact layer
	10	GeNiAu contact
15	20	TiPtAu contact
	50	decoloring absorber layer
	51	carrier capture layer
	52	cladding layer
20	53	current constriction means (AlAs layer)
	54	layer for increasing reflectivity
	100	standing wave field